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JOURNAL OF THE AMERICAN CHEMICAL SOCIETY, vol. 73, no. 12, 24 December 1951, pages 5557-5559; A. P. PHILIPS:  
"Ethanolamides of Some Mono- and Dicarboxylic Acids"

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## Description

This invention concerns the production, purification and isolation of hydroxyamides.

Hydroxyamides are useful as chemical intermediates and chemical crosslinkers.

5     Todate, hydroxyamides have been synthesized by the aminolysis of dimethyl esters by alkanolamines. Isolation and purification of the solid hydroxyamide products is done conventionally either by recrystallization (see for example, J. Coat. Tech., 50(643), 49-55(1978); US-A-4,032,460; US-A-4,076,917; US-A-4,493,909; US-A-4,727,111 and Japanese Patent 56-062895) or by prilling/flaking.

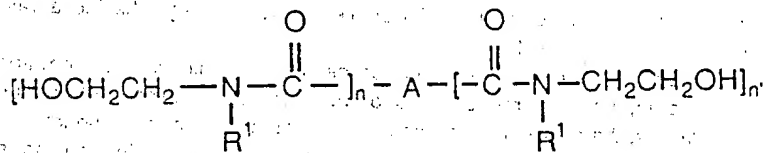
10     Recrystallization is typically performed by dissolving the crude hydroxyamide in a solvent, such as methanol/acetone, cooling the solution to grow the crystals, filtering the product away from the mother liquors, and drying the product until it is free of residual solvent. Alternatively, recrystallization may entail adding solvent to melted hydroxyamide, followed by crystal growth, filtration and drying as described above. With recrystallization, a relatively pure product is obtained. However, the product losses due to dissolution in the solvents used and the complexity of removing residual solvent from the product, as well as recovering solvents for re-use, pose significant disadvantages to this approach.

15     With prilling/flaking, the hydroxyamide must be maintained in a fluid state for several hours until the operation is complete. During this time some of the product in the molten state degrades to undesirable by-products.

20     Another problem associated with the hydroxyamides prepared by the known processes is that they are generally soft, sticky, waxy solids, which typically renders the materials unsuitable for use in powder coatings, such use requiring free-flowing powders.

   The present invention overcomes the problems associated with the known processes for preparing hydroxyamides. Also, the prepared hydroxyamides are useful as crosslinkers in powder coatings based on polyester or acrylate chemistries.

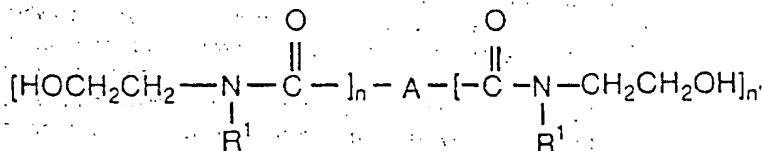
25     In a first aspect, the present invention provides a process for producing hydroxyamides of the formula (I):



I

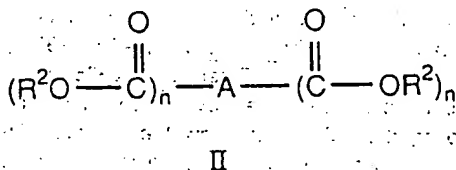
30     wherein n is an integer having a value of 1 to 10; n' is 0 or an integer having a value of 1 or 2; A is a bond, a polyvalent organic radical or, when n' is zero, A may be hydrogen or a monovalent organic radical selected from a saturated or unsaturated alkyl, aryl, carboxy lower alkenyl, lower alkoxy carbonyl lower alkenyl; and R<sup>1</sup> is hydrogen, lower alkyl, or hydroxy lower alkyl; comprising reacting a carboxylic alkyl ester with an alkanolamine at a certain reaction temperature; removing the alcohol by-product compound at atmospheric or reduced pressure; controlling the temperature of the crude reaction mixture until the hydroxyamide crystallizes to form a slurry; maintaining the slurry in the reaction mixture by temperature control (for example, 25° to 200° C, preferably 80° to 115° C) for from about 15 minutes to about 12 hours; and isolating the hydroxyamide.

35     In a second aspect, the present invention provides a process for preparing an hydroxyamide compound of the formula I:

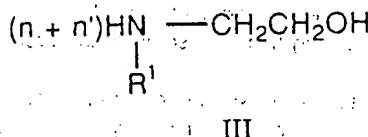


I

wherein  $n$  is an integer of 1 to 10;  $n'$  is 0 or an integer having a value of 1 or 2; A is a bond, a polyvalent organic radical or when  $n'$  is zero, A may be hydrogen or a monovalent organic radical; and  $R^1$  is hydrogen, lower alkyl or hydroxy lower alkyl; comprising reacting a compound of the formula II:



wherein A,  $n$  and  $n'$  are as defined above and R is lower alkyl with a compound of the formula III:



wherein  $R^1$ ,  $R^2$ ,  $n$  and  $n'$  are as defined above, at a temperature in the range of from ambient up to about 200°C, optionally in the presence of a catalyst; controlling the temperature to cause the product (I) to crystallize to form a slurry; maintaining the slurry by temperature control and agitation for from 0.25 to at least about 12 hours; and isolating the hydroxyamide compound.

Preferably, A is a bond, hydrogen, or a monovalent or polyvalent organic radical selected from a saturated or unsaturated alkyl, aryl, carboxy lower alkenyl or lower alkoxycarbonyl lower alkenyl;  $R^1$  is hydrogen, lower alkyl, or hydroxy lower alkyl;  $n$  is an integer having a value of 1 or 2; and  $n'$  is 0 or an integer having a value of 1 or 2.

Preferably, the temperature control of the slurry is maintained at from about 25° to about 200°C.

Preferably, the temperature control of the slurry is maintained at from about 80° to about 115°C.

Preferably, the slurry is maintained for from about 1 to about 3 hours.

Preferably, the hydroxyamide compound is solidified by flaking, prilling, spray drying or casting.

Preferably, A is  $(C_2-C_8)$ alkylene,  $R^1$  is hydroxy lower alkyl and  $n$  and  $n'$  are 1.

The present invention provides a process for producing a high purity solid hydroxyamide by first forming a slurry of the solid hydroxyamide in a liquid melt mixture of the hydroxyamide, amine precursors and other minor process impurities, followed by flaking, prilling, casting, spray drying or other means of solidification to isolate the high purity solid hydroxyamide.

In another aspect, the present invention is used to produce a solid hydroxyamide having the consistency of a free-flowing powder suitable for direct use as a crosslinker in powder coating formulations.

The present invention may be practised by cooling the crude mixture, resulting from the base catalyzed aminolysis of a diester and an alkanolamine, until a thick slurry develops. The temperature of the mixture is then varied to maintain slurry characteristics during the subsequent steps used for solidification (casting, prilling, flaking, and the like).

Solid hydroxyamides produced by the present invention are superior to products produced by prior art methods of recrystallization in that no solvents are involved in the final stages, thus eliminating the additional steps of solvent removal/recovery, and that the physical form characteristics (e.g. free-flowing powder) of the hydroxyamides equal or exceed that obtained from recrystallization.

Furthermore, in contrast to prior art recrystallization methods (which "separate" impurities from the desired product), the present invention uses the slurry environment (solid hydroxyamide in the presence of precursors and by-products) to "convert" some of the by-product impurities to the desired hydroxyamide product. Thus, the slurry conditions drive the chemical reaction towards completion.

The present invention may be used to produce hydroxyamides that are solid at room temperature, i.e., those having melting points above about 25°C.

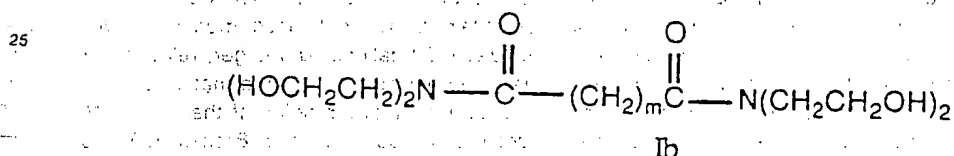
In comparison to the prior art methods, which also employ casting, prilling, or flaking, use of the present invention results in an hydroxyamide product of much higher overall quality (i.e. fewer impurities are present) because the process of the invention does not subject the hydroxyamides to long hold times at elevated temperatures in the molten state (non-slurry conditions) during which times undesirable by-

products form. Also, the operations of filtration and drying, usually associated with recrystallization routes, are eliminated by use of the present invention.

In particular, the hydroxyamides which may be produced by the process of the invention include those represented by formula I (*supra*) but, wherein A is a bond, a polyvalent organic radical or, when n' is zero, A may be hydrogen or a monovalent organic radical, wherein the organic radical is derived from a saturated or unsaturated alkyl radical containing from 1-60 carbon atoms, such as methyl, ethyl, propyl, butyl, pentyl, hexyl, heptyl, octyl, nonyl, decyl, eicosyl, triacontyl, tetracontyl, pentacontyl, hexylcontyl and the like; aryl, for example, mono- and dinuclear aryl such as phenyl, naphthyl and the like; or an unsaturated radical containing one or more ethylenic groups [ >C=C< ] such as ethenyl, 1-methylethenyl; 3-butenyl-1,3-diyl, 2-propenyl-1,2-diyl, carboxy lower alkenyl, such as 3-carboxy-2-propenyl and the like, lower alkoxy carbonyl lower alkenyl such as 3-methoxycarbonyl-2-propenyl and the like; or tri-lower alkyleneamino such as trimethyleamino, triethyleneamino, and the like; R' is hydrogen, lower alkyl of from 1-5 carbon atoms such as methyl, ethyl, n-propyl, n-butyl, sec-butyl, tert-butyl, pentyl and the like or hydroxy lower alkyl of from 1-5 carbon atoms such as hydroxyethyl, 3-hydroxypropyl, 2-hydroxypropyl, 4-hydroxybutyl, 3-hydroxybutyl, 2-hydroxy-2-methylpropyl, 5-hydroxypentyl, 4-hydroxypentyl, 3-hydroxypentyl, 2-hydroxypentyl and the isomers of pentyl; n is an integer having a value of 1 to 10, preferably 1 or 2, and n' is 0 or an integer having a value of 1 or 2 or, when n' is 0, a polymer or copolymer (i.e., n has a value greater than 1 preferably 2-10) formed from the  $\beta$ -hydroxy-alkylamide when A is an unsaturated radical.

Examples of preferred compounds include those wherein A is an alkylene group, preferably (C<sub>2</sub>-C<sub>8</sub>)-alkylene.

Examples of the most preferred compounds fall within the formula Ib:

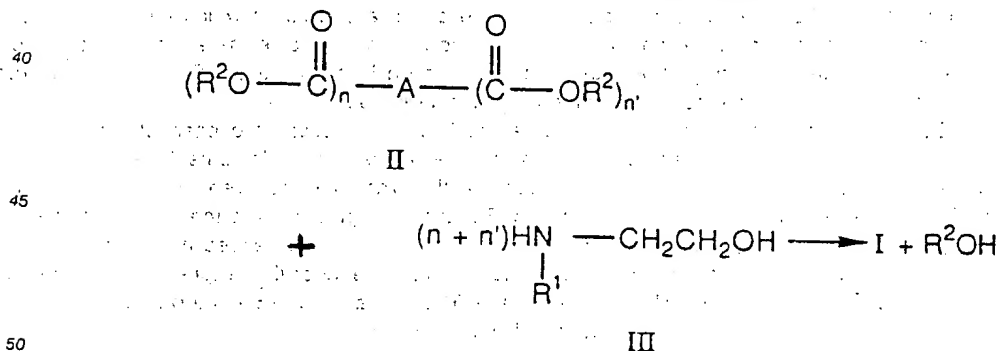


wherein m is 0-10, preferably 2-8.

Specific examples falling within Formula Ib are bis[N,N-di( $\beta$ -hydroxyethyl)]adipamide and bis[N,N-di( $\beta$ -hydroxyethyl)]azelamide.

The  $\beta$ -hydroxyalkylamides (formula I, *supra*) may be prepared by the following reaction scheme I:

#### SCHEME I



wherein A, R<sup>1</sup>, n, and n' are as defined above and R<sup>2</sup> is lower alkyl of from 1-5 carbon atoms such as methyl, ethyl, propyl, n-butyl, tert-butyl, pentyl and the like.

The above scheme represents the aminolysis of an ester of formula II with an amine of formula III at a temperature in the range of from about ambient up to about 200°C. The aminolysis reaction is typically carried out using a molar ratio of amine to ester of 2.0/1, preferably 1.95-2.05/1, and most preferably 1.98-2.02/1. In addition, the water content of the aminolysis reactants is typically controlled to less than 0.5% moisture and preferably to less than 0.1% moisture in order to maintain the activity of any basic catalyst

that may be used and to minimize unwanted hydrolysis of ester reactants. Control of reactant mole ratio and moisture level is typically practised in aminolysis reactions in order to maximize product yield and purity.

Optionally, a basic catalyst may be employed such as, for example, potassium methoxide or butoxide, quaternary ammonium alkoxides (such as tetramethylammonium methoxide and the like), or alkali metal or quaternary ammonium hydroxides and, preferably, in an amount in the range of from 0.1 to 1.0 wt.% based on the weight of the ester. The reaction is preferably conducted at elevated temperatures.

The esters of formula II can be either known compounds or prepared by esterifying the corresponding acid by standard esterifying procedures well-known to those skilled in the art. Among the preferred acids and mixtures thereof which can be employed are oxalic, malonic, succinic, glutaric, adipic, pimelic, suberic, azelaic, sebacic, 1,4-cyclohexane dicarboxylic and the like and alkyl derivatives thereof. Also, there may be employed dimer and trimer acids and mixtures thereof prepared by the polymerization of  $C_{18}$  fatty acids such as a dimer acid with 2 carboxy groups, 36 carbon atoms and an approximate molecular weight of 565 or a trimer acid with 3 carboxy groups, 54 carbon atoms and an approximate molecular weight of 850.

Some representative examples of the amines which can be employed include 2-aminoethanol; 2-methylaminoethanol; and 2-n-butylaminoethanol.

The crude reaction mixture from the aminolysis (i.e. reaction of II with III) is preferably maintained at a temperature of 25-200°C, preferably 80-115°C, until a thick slurry is formed. By manipulating the temperature, the mixture is then maintained in slurry form during subsequent isolation steps (flaking, spray drying, casting, and the like). It is important that the maximum "thickness" of the slurry be maintained during the final isolation steps, and it is important to maintain good agitation of the slurry during these steps. It has been found that maximizing slurry "thickness" (as measured by bulk viscosity of the fluid mixture) unexpectedly maximizes the purity of the final product hydroxyamide.

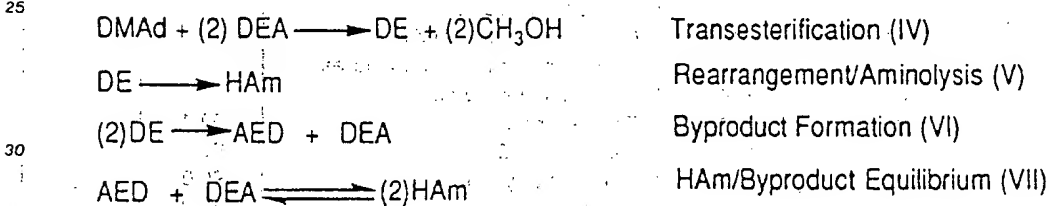
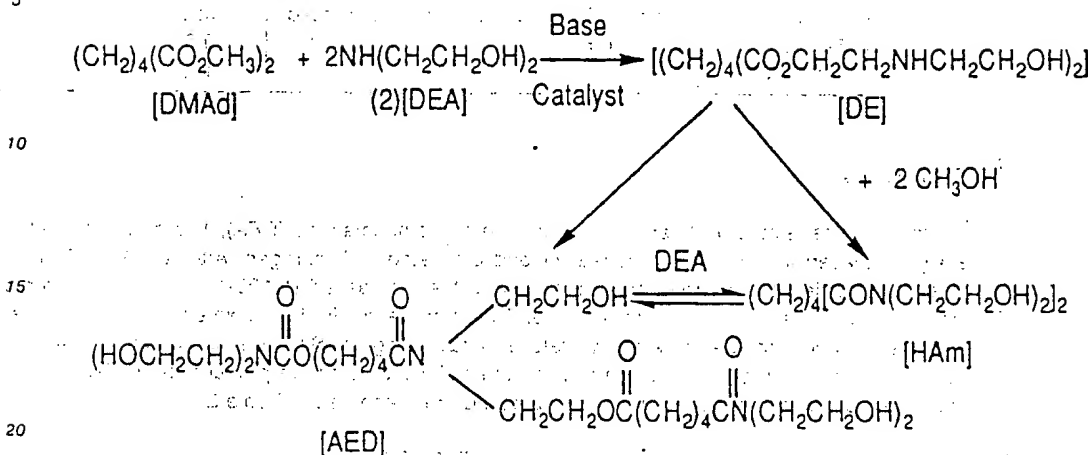
Control of in-process viscosity may be attained by continuous monitoring via on-line viscometer instrumentation. In large-scale reactors (1136 litres (300-gallons) and larger) relative viscosity changes have been found to be most useful; typical changes in bulk viscosity upon formation of a slurry range from 2 to 200 times the bulk viscosity of the reaction mixture prior to formation of the slurry. When laboratory-scale equipment (e.g., 1-liter reactor) is used, viscosities of 300-2,500 cps (Brookfield Viscometer, 100 rpm, 34 sec<sup>-1</sup>) are suitable for producing high purity hydroxyamides, with 600-2,000 cps being a preferred viscosity range.

In-process pressure is not critical to the use of the invention and so vacuum or elevated pressures may be used to satisfy individual process requirements. However, it is preferable to use a slight vacuum (50-300 mm Hg) to remove residual methanol (or other alcohol by-products) from the aminolysis reaction. Hold times may vary widely depending on the vacuum conditions and temperatures employed for the aminolysis; thereafter the temperature of the crude liquid reaction mixture is controlled in such a way to form the thick slurry. The thick slurry condition is maintained with good agitation and temperature control from about 15 minutes up to at least about 12 hours, preferably 1-3 hours, in order to achieve maximum purity of the hydroxyamide. The aminolysis may also be carried out in a solvent, in which case the solvent should be removed prior to formation of the slurry. Moreover, solvent may enable the aminolysis to be conducted at lower temperatures, resulting in less by-product formation in some cases. Practice of the process of the invention may be by batch, continuous or semi-continuous modes.

Scheme II, represented below, presents an outline of the postulated chemistry of the process steps involved in the use of the invention, in which the reaction of dimethyladipate (DMA<sub>d</sub>) and diethanolamine (DEA) is used for illustrative purposes. In Scheme II (*infra*), it is believed that the initial base-catalyzed (KOH, or other strong bases) transesterification (Equation IV) rapidly forms the theoretical diester intermediate (DE) along with methanol. DE is then believed to convert to the desired hydroxyamide (HAM) product (Equation V) or the amide-ester dimer, AED (Equation VI). The latter (in the presence of DEA) subsequently establishes an equilibrium with HAM (Equation VII). The formation of AED is a primary source of impurity in final product HAM and also the main cause of low HAM yield.

During the aminolysis reaction, all of the Scheme II components are present simultaneously in solution. As the methanol is stripped off, the HAM may begin to "crystallize" from the mixture, i.e., to form a solid in liquid (slurry), due to its lesser solubility in the reaction medium in the absence of methanol. As additional HAM crystallizes from the molten slurry mixture, the equilibrium is shifted toward HAM at the expense of DEA, DE, and AED, all of which are undesirable components in the HAM product.

### SCHEME II



35 The crystallization of HAm is relatively slow, therefore, extended hold times tend to produce purer product and more viscous slurries. The viscosities of the slurries should be maintained as high as possible to maximize the purity and yield of the HAm, but the viscosities should not be so high that the reaction mixture completely solidifies ("sets up"), e.g., above 2,500 cps absolute viscosity at 80 °C in small-scale laboratory reactors.

The present invention will now be described by way of examples.

### EXAMPLE 1

A mixture of diethanolamine (DEA), 131 g, and potassium hydroxide (KOH), 0.5 g, is placed in a 500-ml glass reactor and blanketed with nitrogen. This mixture is heated to 100 °C under 205 mm Hg vacuum with stirring, at which point dimethyladipate (DMAd) is introduced into the mixture dropwise. The DMAd (106 g) is added over a 4 hour period during which period, methanol is simultaneously distilled from the reaction mixture. Within one hour after completion of the DMAd addition, the reaction mixture develops the appearance of a thick, white slurry. The slurry is maintained at 100-103 °C for an additional 1.75 hours. The HAM product is isolated by pouring the slurry into an aluminum dish at 20-25 °C.

### EXAMPLE 2 (Comparative)

In a manner similar to Example 1, the aminolysis is repeated and the reactor temperature is maintained at 93°C such that the reaction mixture maintains its homogeneous character without forming a slurry after the DMA<sub>d</sub> addition. The reaction solution is then poured into an aluminum dish at 20-25°C to isolate the HAM product.

Analytical data on the HAM products obtained by the processes of Example 1 (present invention) and Example 2 (prior art/comparative) are presented in Table I.

TABLE I

	Example 1 Present Invention	Example 2 Comparative
Physical Appearance:	free-flowing, white chalky solid	sticky, white solid
% Residual DEA:	5.3	9.0
M.P. (°C):	124	117

## EXAMPLE 3

In a manner similar to Example 1, a mixture of diethanolamine (DEA), 129 g, and potassium t-butoxide, 2.4 g, is placed in a 500-ml glass reactor and blanketed with nitrogen. After DMAc (106 g) is added and methanol distilled off, the reaction temperature is then increased to 108-110 °C and held for 30 minutes to slowly convert the HAM to its molten state. The temperature is then lowered to 87 °C over a period of 25 minutes at which point a thick slurry state is obtained again. Samples are withdrawn from the reactor at each stage of this process, allowed to cool and solidify to produce product HAM. Experimental conditions and analytical data obtained from on-line sampling are presented in Table 2.

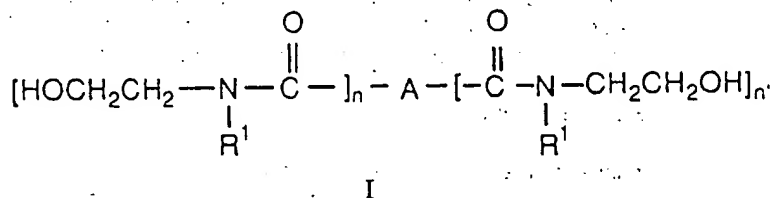
TABLE 2

Time (min)	Temp (°C)	Operation/Comments	% HAM	% DEA	AED/HAM
0	84	Start DMAc addition			
30	79	Reaction mixture cloudy			
50	84	Formation of slurry, temp increased			
60	108	DMAc addition complete			
75	110	Thick slurry (A)	90.4	1.7	0.043
90	109	Thick slurry (B)	90.8	1.6	0.044
120	109	Thinner slurry (C)	90.0	1.9	0.056
150	108	Cloudy, no slurry (D)	84.8	2.4	0.064
180	108	Cloudy, no slurry (E), temp lowered	83.1	3.1	0.085
205	87	Slurry (F)	90.0	1.6	0.042
(HAM and AED/HAM ratios are determined by HPLC analyses.)					

The data indicate that "slurry" conditions (samples A, B, C, and F) are conducive to high purity product (90+ % HAM, < 2% DEA, lower AED/HAM ratio), whereas "molten" conditions (samples D and E), representing the comparative prior art, are conducive to low purity product (< 85% HAM, > 2% DEA, higher AED/HAM ratio).

## Claims

1. A process for producing hydroxyamides of the formula (I):



wherein n is an integer having a value of 1 to 10; n' is 0 or an integer having a value of 1 or 2; A is a bond, a polyvalent organic radical or, when n' is zero, A may be hydrogen or a monovalent organic radical selected from a saturated or unsaturated alkyl, aryl, carboxy lower alkenyl, lower alkoxy carbonyl lower alkenyl; and R<sup>1</sup> is hydrogen, lower alkyl, or hydroxy lower alkyl;

comprising

reacting a carboxylic alkyl ester with an alkanolamine at a certain reaction temperature;

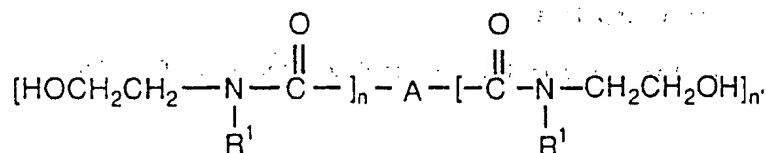
removing the alcohol by-product compound at atmospheric or reduced pressure;

controlling the temperature of the crude reaction mixture until the hydroxyamide crystallizes to form a slurry;

maintaining the slurry in the reaction mixture by temperature control (for example at from about 25° to about 200°C, preferably about 80° to about 115°C) for from about 15 minutes to about 12 hours (preferably about 1 to about 3 hours); and

isolating the hydroxyamide.

2. A process for preparing an hydroxyamide compound of the formula I:

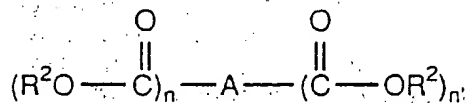


I

wherein n is an integer of 1 to 10; n' is 0 or an integer having a value of 1 or 2; A is a bond, a polyvalent organic radical or when n' is zero, A may be hydrogen or a monovalent organic radical; and R<sup>1</sup> is hydrogen, lower alkyl or hydroxy lower alkyl;

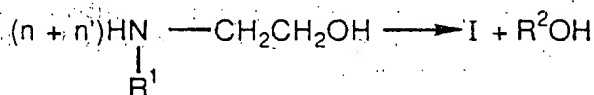
comprising

reacting a compound of the formula II:



II

wherein A, n and n' are as defined above and R is lower alkyl with a compound of the formula III:



III

wherein R<sup>1</sup>, R<sup>2</sup>, n and n' are as defined above,

at a temperature in the range of from ambient up to about 200°C, optionally in the presence of a catalyst; controlling the temperature to cause the product (I) to crystallize to form a slurry; maintaining the slurry by temperature control and agitation for from 0.25 to at least about 12 hours; and isolating of the hydroxyamide compound.

3. The process of claim 1 or claim 2 wherein A is a bond, hydrogen, or a monovalent or polyvalent organic radical selected from a saturated or unsaturated alkyl, aryl, carboxy lower alkenyl or lower alkoxy carbonyl lower alkenyl; R<sup>1</sup> is hydrogen, lower alkyl, or hydroxy lower alkyl; n is an integer having a value of 1 or 2; and n' is 0 or an integer having a value of 1 or 2.

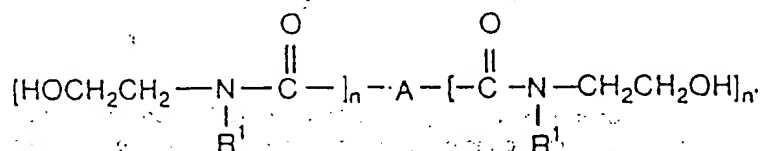
4. The process of any one of the preceding claims wherein the temperature control of the slurry is maintained at from about 25° to about 200°C.



5. The process of claim 4 wherein the temperature control of the slurry is maintained at from about 80° to about 115° C.
6. The process of any one of the preceding claims wherein the slurry is maintained for from about 1 to about 3 hours.
7. The process of any one of the preceding claims wherein the hydroxyamide compound is solidified by flaking, prilling, spray drying, or casting.
8. The process of any one of the preceding claims wherein A is (C<sub>2</sub>-C<sub>8</sub>)alkylene; R<sup>1</sup> is hydroxy lower alkyl and n and n' are 1.

# Patentansprüche

1. Verfahren zum Herstellen von Hydroxyamiden der Formel (I):



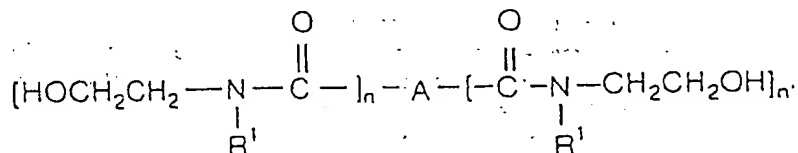
wobei n eine ganze Zahl mit einem Wert von 1 bis 10 ist; n' 0 oder eine ganze Zahl mit einem Wert von 1 oder 2 ist; A eine Bindung, ein mehrwertiges organisches Radikal ist oder, wenn n' 0 ist, kann A Wasserstoff oder ein einwertiges organisches Radikal ausgewählt aus einem gesättigten oder ungesättigten Alkyl, Aryl, Carboxy-Niederalkenyl, Niederalcoxycarbonyl-Niederalkenyl sein; und R<sup>1</sup> Wasserstoff, Niederalkyl oder Hydroxy-Niederalkyl ist; umfassend:

Umsetzung eines Carbonsäurealkylesters mit einem Alkanolamin bei einer bestimmten Reaktionstemperatur;

Entfernen der alkoholischen Nebenproduktverbindung bei atmosphärischem oder reduziertem Druck; Steuern der Temperatur des Rohreaktionsgemischs bis das Hydroxyamid zur Bildung einer Aufschlammung kristallisiert;

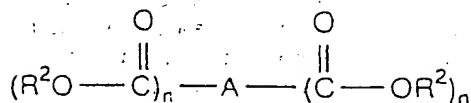
Beibehalten der Aufschlammung im Reaktionsgemisch durch Temperaturregung (z.B. von ungefähr 25° C bis ungefähr 200° C, vorzugsweise ungefähr 80° C bis ungefähr 115° C) für ungefähr 15 min bis ungefähr 12 h (vorzugsweise ungefähr 1 bis ungefähr 3 h); und Isolieren des Hydroxyamids.

2. Verfahren zum Herstellen einer Hydroxyamidverbindung der Formel I:



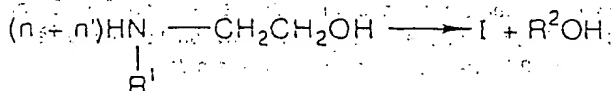
wobei n eine ganze Zahl von 1 bis 10 ist; n' 0 oder eine ganze Zahl mit einem Wert von 1 oder 2 ist; A eine Bindung, ein mehrwertiges organisches Radikal, oder wenn n' 0 ist, kann A Wasserstoff oder ein einwertiges organisches Radikal sein; und R<sup>1</sup> Wasserstoff, Niederalkyl oder Hydroxy-Niederalkyl ist; umfassend:

Umsetzung einer Verbindung der Formel II:



II

worin A, n and n' so wie oben definiert sind und R<sup>2</sup> Niederalkyl ist, mit einer Verbindung der Formel III:



III

worin R<sup>1</sup>, R<sup>2</sup>, n and n' wie oben definiert sind,

bei einer Temperatur im Bereich von Raumtemperatur bis ungefähr 200 °C, wahlweise in Anwesenheit eines Katalysators; Steuern der Temperatur um das Produkt (I) zur Kristallisation zur Bildung einer Aufschlämmung zu bewegen; Beibehalten der Aufschlämmung durch Temperatursteuerung und Rühren für 0,25 bis mindestens ungefähr 12 h; und Isolieren der Hydroxyamidverbindung.

3. Verfahren nach Anspruch 1 oder 2, wobei A eine Bindung, Wasserstoff oder ein einwertiges oder mehrwertiges organisches Radikal ausgewählt aus gesättigtem oder ungesättigtem Alkyl, Aryl, Carboxy-Niederalkenyl oder Niederalcoxycarbonyl-Niederalkenyl ist; R<sup>1</sup> Wasserstoff, Niederalkyl oder Hydroxy-Niederalkyl ist; n eine ganze Zahl mit einem Wert von 1 oder 2 ist; und n' 0 oder eine ganze Zahl mit einem Wert von 1 oder 2 ist.

4. Verfahren nach einem der vorhergehenden Ansprüche, wobei die Temperatursteuerung der Aufschlämmung von ungefähr 25 ° bis ungefähr 200 °C gehalten wird.

5. Verfahren nach Anspruch 4, wobei die Temperatursteuerung der Aufschlämmung von ungefähr 80 ° bis ungefähr 115 °C gehalten wird.

6. Verfahren nach einem der vorhergehenden Ansprüche, wobei die Aufschlämmung von ungefähr 1 bis ungefähr 3 h beibehalten wird.

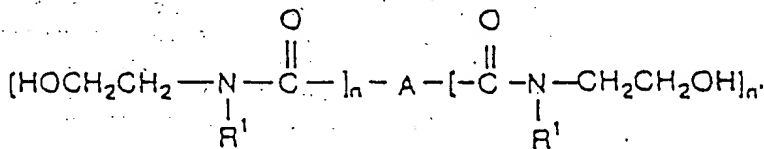
7. Verfahren nach einem der vorhergehenden Ansprüche, wobei die Hydroxyamidverbindung durch Ausflocken, Sprühkristallisation, Sprühtrocknung oder Gießen verfestigt wird.

8. Verfahren nach einem der vorhergehenden Ansprüche, wobei A (C<sub>2</sub>-C<sub>8</sub>)Alkyl ist; R<sup>1</sup> Hydroxy-Niederalkyl ist und n und n' 1 sind.

#### Revendications

1. Procédé de préparation d'hydroxyamides de formule

(I):



I

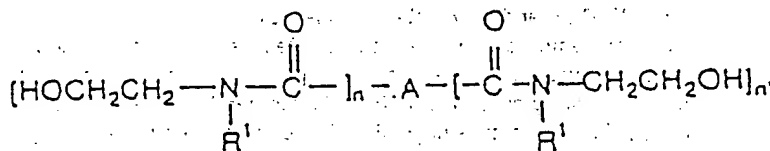
dans laquelle n est un nombre entier valant de 1 à 10; n' vaut 0 ou un nombre entier valant 1 ou 2; A est une liaison, un radical organique polyvalent ou lorsque n' vaut 0, A peut être un hydrogène ou un radical organique monovalent choisi parmi alkyle saturé ou insaturé, aryle, carboxyalcényle inférieur, alkoxy inférieur-carbonyl-alcényle inférieur; et R<sup>1</sup> est un hydrogène, alkyle inférieur ou hydroxy-alkyle inférieur;

dans lequel on fait réagir un alkyl-ester carboxylique avec une alkanolamine à une certaine température réactionnelle;

on enlève le composé alcool sous-produit à la pression atmosphérique ou à une pression réduite;

on règle la température du mélange réactionnel brut jusqu'à ce que l'hydroxyamide cristallise pour former une bouillie; on maintient la bouillie dans le mélange réactionnel par régulation de la température (par exemple entre environ 25° et environ 200°C, de préférence entre environ 80° et environ 115°C) pendant une durée allant d'environ 15 minutes à environ 12 heures (de préférence environ 1 à environ 3 heures) et on isole l'hydroxyamide.

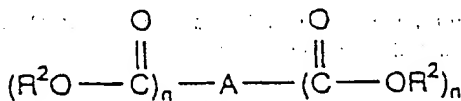
2. Procédé de préparation d'un composé hydroxyamide de formule (I) :



I

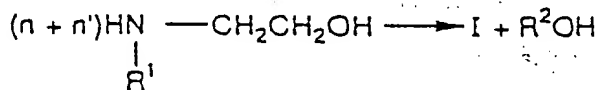
dans laquelle n est un nombre entier allant de 1 à 10; n' vaut 0 ou un nombre entier ayant une valeur de 1 ou 2; A est une liaison, un radical organique polyvalent ou lorsque n' vaut 0, A peut être un hydrogène ou un radical organique monovalent; et R<sup>1</sup> est un hydrogène, alkyle inférieur ou hydroxy-alkyle inférieur;

dans lequel on fait réagir un composé de formule II:



II

dans laquelle A, n et n' sont tels que définis ci-dessus et R<sup>2</sup> est un alkyle inférieur, avec un composé de formule III:



III

dans laquelle R<sup>1</sup>, R<sup>2</sup>, n et n' sont tels que définis ci-dessus,

à une température allant de la température ambiante jusqu'à environ 200°C, facultativement en présence d'un catalyseur; on règle la température pour provoquer la cristallisation du produit (I) afin de former une bouillie; on maintient la bouillie par régulation de la température et agitation entre 0,25 et au moins environ 12 heures; et on isole le composé hydroxyamide.

3. Procédé de la revendication 1 ou de la revendication 2 dans lequel A est une liaison, un hydrogène, ou un radical organique monovalent ou polyvalent choisi parmi alkyle saturé ou insaturé, aryle, carboxyalcényle inférieur ou alkoxy inférieur-carbonyl-alcényle inférieur; R<sup>1</sup> est un hydrogène, alkyle

inférieur, ou un hydroxy-alkyle inférieur, n est un nombre entier valant 1 ou 2; n' vaut 0 ou un nombre entier valant 1 ou 2.

4. Procédé de l'une quelconque des revendications précédentes dans lequel la régulation de température de la bouillie est maintenue entre environ 25° et environ 200° C.
5. Procédé de la revendication 4 dans lequel la régulation de la température de la bouillie est maintenue entre environ 80° et environ 115° C.
6. Procédé de l'une quelconque des revendications précédentes dans lequel la bouillie est maintenue pendant environ 1 à environ 3 heures.
7. Procédé de l'une quelconque des revendications précédentes dans lequel on solidifie le composé hydroxyamide par écaillement, granulation, séchage par pulvérisation ou coulage.
8. Procédé de l'une quelconque des revendications précédentes dans lequel A est un alkylène en C<sub>2</sub> à C<sub>8</sub>; R' est un hydroxy-alkyle inférieur et n et n' vaut 1.